Arbegast Materials Processing and Joining Laboratory



An Investigation into Microstructure & Mechanical Behavior of Al Alloy Coatings Deposited by Cold Spray Processing Ph.D. Dissertation Defense Reza Rokni

Committee Members:

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South Dakota School of Mines and Technology

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Outline

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- ➢ Introduction
- ➢ Background
- > Motivation for this work
- Results from this work
 - ✓ Microstructure characterization
 - ✓ Mechanical properties
- Conclusions





Cold gas dynamic spraying or CS is a unique solid-state materials consolidation process that utilizes high velocity particles impinging upon a substrate to build up coatings and/or freestanding structures without the use of combustion fuels.

Main Parameters:

- ✓ Main Gas Pressure
- ✓ Gas Temperature
- ✓ Particle Velocity
- ✓ Particle Size
- ✓ Main Gas Flow Rate
- ✓ Powder Feed Rate

Applications:

- ✓ Dimensional Restoration
- ✓ Wear Resistant Coatings
- ✓ Casting Repair
- ✓ Electronics (metalizing ceramics)
- ✓ Fabrication of Parts
- ✓ Novel Weapon Systems

The major problem with cold sprayed coatings is having inferior mechanical properties in compared with bulk materials.



Background





R. Morgan, P. Fox, J. Pattison, C. Sutcliffe, W. O' Neill, Mater. Letters 58 (2004) 1317–1320.



CS imposes high degree of deformation on the powder particles and generates an inhomogeneous microstructure.

T. Van Steenkiste, J. Smith, R. Teets, Surf. Coat. Technol. 154 (2002) 237-252.



Background







H. Assadi et al. Acta Mater. 51 (2003) 4379–4394.

K. Kim, M. Watanabe, S. Kuroda, Surf. Coat. Technol. 204 (2010) 2175–2180.

(b) Generation of a high impact region and the resultant intensive shear stress(c) Formation of dislocation structures and pancaked grains(d) Recrystallized grains in some areas





Addressing Concerns About:

- ✓ Limited attention has been dedicated to microstructural study of cold spray processed (CSP) alloys.
- ✓ Limited study on characteristics of the microstructure in different areas of the deposit.
- ✓ Lack of information in the literature on formation mechanisms for the microstructural features in deposited material.
- ✓ Lack of enough data on local and bulk mechanical properties.

There is a need for a systematic study relating: Processing - Microstructure - Mechanical Behavior.



Research Thrusts





- ✓ Different aluminum alloys, 6061, 5083 and 7075
 ✓ Non-isothermal Annealing
 ✓ Heat treatments
- ✓ Heat treatments

Characterization
 ✓ Grain structure (EBSD/BSE)
 ✓ Precipitates (SEM/DSC/EDS)
 ✓ Dislocation density (XRD/TEM)
 ✓ Lattice parameter (XRD)
 ✓ Microstrain (XRD)

Microstructure

Deformation Behavior

- ✓ Microhardness
- ✓ Nanohardness
- ✓ Microtensile



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Gas-atomized 6061 Al powder and the CSP deposit



Powder Morphology and Structure



Particle Size Analysis

Size range of 5-50 μm and average size of 38.7 μm





≻Powder grains are not relaxed

>Medium and uniform DD

➢Solute segregation







GB Solute segregation









Si Ka1

Mg Ka1_2

1µm

> More extreme solute segregation at the grain boundaries

Element	Wt% (P. Gbs)	Wt% (P. Matrix)	Wt% (CSP layer Matrix)
Al	88.6	97.4	98.4
Mg	2.2	1.0	0.7
Si	4.5	1.0	0.7
Fe	3.2	-	-
Cu	1.5	0.6	0.2
Total	100	100	100

M.R. Rokni, C.A. Widener, V.R. Champagne, Microstructural stability of ultrafine grained cold sprayed 6061 Al alloy, Appl. Surf. Sci. 290 (2014) 482-489.

M.R. Rokni, C.A. Widener, S.P. Ahrenkiel, B.K. Jasthi, V.R. Champagne, Annealing Behavior of 6061 Al Deposited by High Pressure CS, Surface Engineering 30 (2014) 361-368.



CSP deposition (EBSD)



✓ The microstructure of the deposition is *inhomogeneous*.

➢ No preferred texture

➤ Less deformation around the center

➢ UFG structure at the particle interfaces

M.R. Rokni, C.A. Widener, V.R. Champagne, Microstructural Evolution of 6061 Al Gas-Atomized Powder and High-Pressure Cold-Sprayed Deposition, Journal of thermal spray technology 23 (2014) 514-524.









Nanocrystalline 5083 Al powder and the CSP deposit



5083 Nanocrystalline





> Incoming grain structure is important.

✓ Different microstructural features
✓ Different deformation mechanisms
✓ Different mechanical behavior



M.R. Rokni, C.A. Widener, A.T. Nardi, V.K. Champagne, Nano crystalline high energy milled 5083 Al powder deposited using CS, Applied Surface Science 305 (2014) 797-804.





Key Messages:

- Cold spray can be a promising technique for producing bulk alloy materials.
- The gas-atomized Al alloy powders contain grain boundary solute segregation retained in deposition.
- The microstructure of deposited materials is inhomogeneous and includes distinct microstructural regions.





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Gas-atomized 7075 Al powder and CSP deposit









Why Al 7075?

- Aluminum is an abundant resource
- > Relatively cheap
- > High stiffness/density and strength/density ratios
- Damage tolerant
- Corrosion resistant compared with conventional alloys

ApplicationsGears and shaftsAircraftAerospace and defense applications





- ✓ 7075 Al coatings were produced using commercially available gas-atomized 7075 Al powder.
- ✓ Microstructural characterization of the as-received powder and the coatings via different microscopy techniques including, TEM, SEM and EBSD.
- ✓ In-situ hot-stage TEM from room temperature to 450° C.
- ✓ Differential scanning calorimetry (DSC)
- ✓ X-ray diffraction profiles (XRD)

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- ✓ Energy-dispersive X-ray spectroscopy (EDS)
- ✓ Microhardness & Nanohardness testing
- ✓ Micro-tensile testing method
- The main objective of this work was to study the microstructure and mechanical properties of cold sprayed 7075 coating in as-deposited and heat treated conditions.



Background – Solute Segregation





 $18.6 \pm 8.2 \,\mu\text{m}$ in size Surface structure of a ~1-3 μm sized grains

evidence for GB solute segregation





Background – Solute Segregation



✓ Retention of solute segregation at the grain boundaries (GBs) of the cold sprayed deposition.





TEM study of the powder



- ✓ Some internal UFG and even nano structures in powder particles
- Moderate density of dislocations and dislocation substructures
- ✓ Internal HAGBs (black lines) and LAGBs (white lines)







Overall structure of the CSP layer





✓ Elongation of spherical particles

 \checkmark No evidence of voids or porosity



Overall structure of the CSP layer





near the interface

 Presence of more porosity and void in the top portion of the deposit



Overall structure of the CSP layer





EBSD characterization









EBSD characterization



✓ A limited number, compared to particle interiors, of LAGBs (dislocations) in these areas.





EBSD characterization



✓ A limited number, compared to particle interiors, of LAGBs (dislocations) in these areas.





EBSD characterization



✓ A limited number, compared to particle interiors, of LAGBs (dislocations) in these areas.





Main formation mechanisms



Geometric DRX (GDRX)







- 1) The serrated HAGBs (thick lines) become closer.
- 2) The subgrain size remains approximately constant.
- 3) Eventually the high angle boundaries (HAGBs) impinge.

F.J. Humphreys, M. Hatherly, Recrystallization and Related Annealing Phenomena. Oxford, 2004.

Microstructure of the CSP layer



✓ Some elongated grain structures at particle/particle boundaries





Microstructure of the CSP layer



✓ Subdivided into pancaked subgrains by some LAGBs





Main formation mechanisms



✓ Geometric DRX (GDRX) is one of the main mechanisms.







School of Mines & Technology Structure Evolution of GBs

 \checkmark 3 types of boundaries:

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- 1- Polygonized dislocation wall (<1°)
- 2- Partially transf. boundary (1-5°)
- 3- Grain boundary (>15°)



This is evidence of continuous DRX (CDRX). Therefore, a combination CDRX and GDRX is responsible for formation of UFG structures in the microstructure.

Microstructural evolution of 7075 Al gas atomized powder and high-pressure cold sprayed deposition, Surface and Coatings Technology 251 (2014) 254-263.

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Precipitates in the Deposition



 ✓ A variety of different precipitates composed of various amounts of Al, Zn, Mg, Cu and Si

✓ η (MgZn₂) and Mg(Zn,Cu,Al)₂

















Precipitates in the Deposition



- ✓ Low sized grains: located primarily at grain boundaries
- ✓ High sized grains: distributed throughout the grain interior
- ✓ Due to volume for dislocations interaction and more nucleation sites







Nanohardness results





M. R. Rokni, C. A. Widener, G. A. Crawford, M. K. West, An Investigation into Microstructure & Mechanical Properties of cold sprayed 7075 Al deposition, Materials Science & Engineering A 625 (2015) 19-27.

Nanohardness results





 1.53 ± 0.30

 2.01 ± 0.09



Details of Microstructure (TEM)

Final microstructure After Annealing

✓ Equiaxed grains with well-defined, straight GBs, unlike the inhomogeneous microstructure observed in the as-deposited coating.

Final microstructure After Annealing

- \checkmark Many of the grains are free of dislocations
- \checkmark Some grains still contain a medium dislocation density
- \checkmark Residual stress relief through the annealing process.

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Particle interiors: ✓ Not that much affected

- ✓ Significant dislocation density
- After Annealing 1 μm

Final microstructure (UFG structure)

UFG structures:

- ✓ Relatively unaffected by the annealing process.
- ✓ Some reduction in overall dislocation density, improved GB definition.

Final Microstructure (Pancaked Str.)

Pancaked structures:

- ✓ Significant recrystallization during the annealing
- ✓ Developing an UFG structure as opposed to pancaked structures

Non-isothermal In-situ TEM Heating

1) Dislocation movement

3) Dislocation free microstructure/ RX

2) Annihilation of dislocations and substructures

4) precipitation and Growth of precipitates

Microstructure During Annealing

From RT to 225°C: ✓ Dislocation movement ✓ Retention of pancaked structure.

Microstructure During Annealing

At 280°C: collapse of lamellar structure At 370°C: some evidence of recrystallization At 450°C: *Limited grain growth because of grain boundary precipitation*

Differential Scanning Calorimetry

✓ An endothermic peak at region I → Dissolution of G-P zones

✓ Exothermic peak at region II → Formation of η'/η

✓ Endothermic peak at region III \rightarrow Dissolution of all phases

 No strengthening precipitates after about 370°C in the microstructure

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M.R. Rokni, C.A. Widener, G.A. Crawford, Microstructure and Mechanical Properties of cold sprayed 7075 Deposition during Non-isothermal Annealing, submitted to Acta Materialia.

X-ray Diffraction Profile

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Microstructure Analysis

(1) A noticeable increase in LP between due to the dissolution of G-P zones
 (2) significant decrease in LP due to the formation of η'/η precipitates
 (3) An increase in LP due to dissolution of all phases in the matrix.

Microstructure Analysis

- ✓ Continual decrease in the DD and microstrain by temperature
 - due to more driving force by annealing
- ✓ Dislocation rearrangement in low temperatures
- ✓ More mobility of dislocations towards higher temperatures

Mechanical Behavior

Mechanical Behavior

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There are four strengthening mechanisms that may play a role in the microhardness evolution of this material during non-isothermal annealing:

- \checkmark Grain boundary strengthening
- \checkmark Solid solution strengthening
- ✓ Precipitate strengthening
- ✓ Strain hardening.

Hall–Petch equation

$$\sigma_y = \sigma_0 + \frac{k_y}{\sqrt{d}}$$

CSP 7075 deposition $\sim 500 \text{ nm}$ Solution treated bulk 7075 alloy $100.6 \pm 23.2 \,\mu\text{m}$ 160 MPa

Mechanical Behavior

 ✓ Micro-tensile samples were heat treated to different commercial HTs of 7075 Al alloy: ⁷⁰⁰ ⊥

1-As-deposited (AD)

- 2- T6
- 3- 7X

4- T73

5- Stress relief (SR)

6- Annealing

7- Solution treating + T6 (SS+T6)

Mechanical Properties of HTed Samples

 \checkmark The lowest UTS and ductility for the AD condition.

Due to significant imposed cold plastic deformation Largely decreased strain-hardening ability

- 1. This research detailed the microstructure evolution and mechanical properties of CSP 7075 Al deposition.
- 2. Significant solute element segregation was observed at grain boundaries of particles.
- 3. HPCS resulted in the formation of a high quality deposition with limited porosity and inter-particle voids.
- 4. The deposition was characterized by two distinct regions: particle interfaces (UFG & pancaked) and particle interiors.
- 5. The formation of the UFG structure was attributed to a combination of CDRX and GDRX.

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- 6. Microstructural stability of the distinct regions was evaluated during non-isothermal annealing from RT to 450°C.
- 7. The pancaked regions experience recrystallization and are converted to UFG structures during the annealing.
- 8. The microhardness stays high even towards the end of annealing due to grain boundary strengthening mechanism.
- 9. The mechanical properties of the deposition can be substantially improved with low and high temperature heat treatments
- 10. This happens due to precipitation of strengthening phases and metallurgical bonding.

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- > My advisers, Dr. Widener & Dr. Crawford
- Army Research lab (ARL)

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- > My committee memebers: Dr. M. West, Dr. P. Ahrenkiel & B. Jasthi
- SDMS&T microstructural characterization team: Dr. P. Ahrenkiel and Dr. E. Duke.
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- > My family of brothers and sisters here in Rapid City
- > My mother, father, brother, and sisters

Contribution to Science

1. M.R. Rokni, C.A. Widener, A.T. Nardi, V.K. Champagne, Nano crystalline high energy milled 5083 Al powder deposited using CS, Applied Surface Science 305 (2014) 797-804.

2. M.R. Rokni, C.A. Widener, V.R. Champagne, Microstructural Evolution of 6061 Al Gas-Atomized Powder and High-Pressure Cold-Sprayed Deposition, J thermal spray technology 23 (2014) 514-524.

3. M.R. Rokni, C.A. Widener, S.P. Ahrenkiel, B.K. Jasthi, V.R. Champagne, Annealing Behavior of 6061 Al Deposited by High Pressure CS, Surface Engineering 30 ,(2014) 361-368.

4. M.R. Rokni, C.A. Widener, V.R. Champagne, Microstructural stability of ultrafine grained cold sprayed 6061 Al alloy, Applied Surface Science 290 (2014) 482-489.

5. M.R. Rokni, C.A. Widener, G.A. Crawford, Microstructure and mechanical properties of cold sprayed 6061 Al in as-sprayed and different heat treated conditions, Under Preparation.

6. M.R. Rokni, C.A. Widener, G.A. Crawford, Microstructural evolution of 7075 Al gas atomized powder and high-pressure cold sprayed deposition, Surf. Coat. Technol. 251 (2014) 254-263.

7. M.R. Rokni, C.A. Widener, The strain-compensated consetitutive equation for high temperature flow behavior of a 7075 Al alloy, J Materials Engineering & Performance 23 (2014) 4002-4009.

8. M. R. Rokni, C. A. Widener, G. A. Crawford, M. K. West, An Investigation into Microstructure & Mechanical Properties of cold sprayed 7075 Al deposition, Mater. Sci. Eng. A 625 (2015) 19-27.

9. M.R. Rokni, C.A. Widener, G.A. Crawford, Microstructure and Mechanical Properties of cold sprayed 7075 Deposition during Non-isothermal Annealing, submitted to Acta Materialia.

10. M.R. Rokni, C.A. Widener, G.A. Crawford, The effects of post CS heat treatments on microstructure & Mechanical properties of 7075 Al depositions, Under preparation.

Success is achieved and maintained by those who develop a burning desire for their high goals and then keep on trying with positive mental attitude.

"Success through a positive mental attitude"

By Napoleon Hill

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Thank you for your attention!

Contact:

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